



Tu2C-3

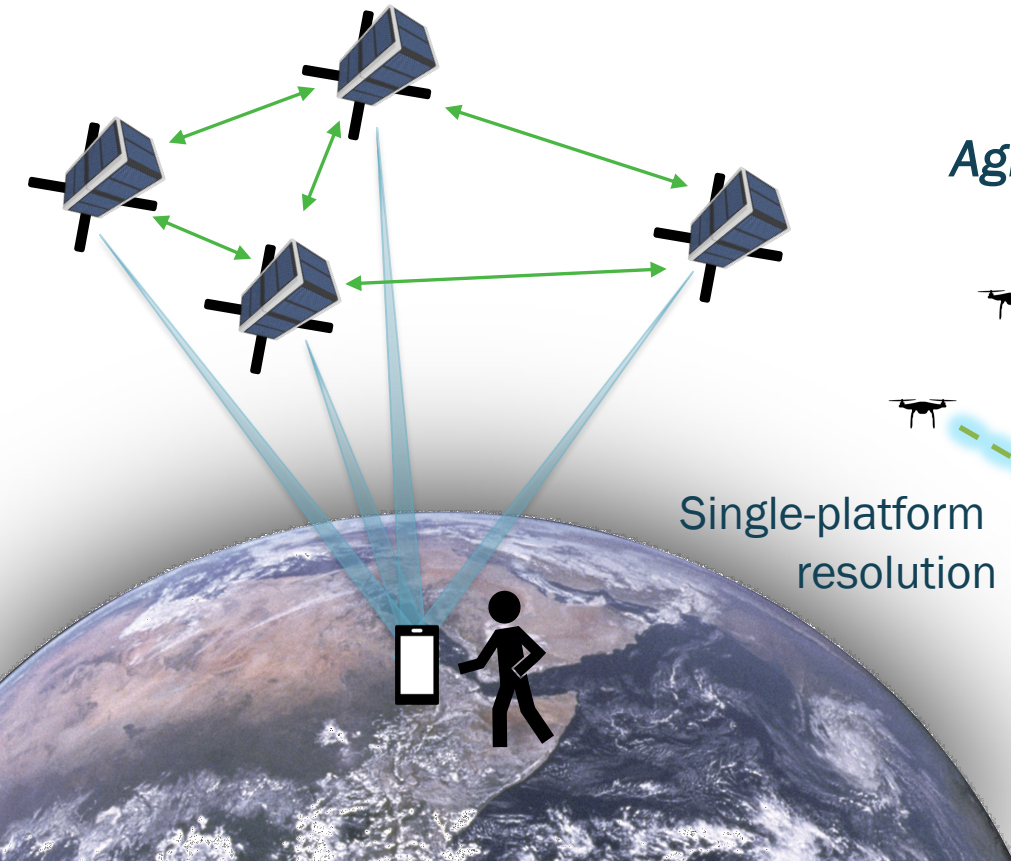
# High Accuracy Wireless Time-Frequency Transfer for Distributed Phased Array Beamforming

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and Jeffrey A. Nanzer**

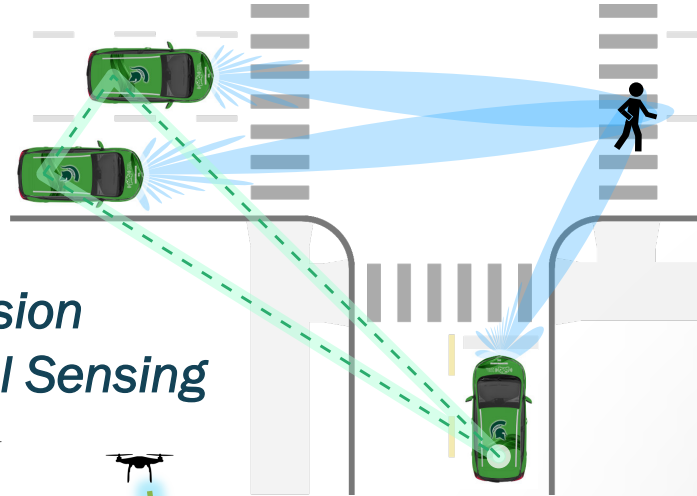
Electrical and Computer Engineering  
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# Distributed Phased Arrays

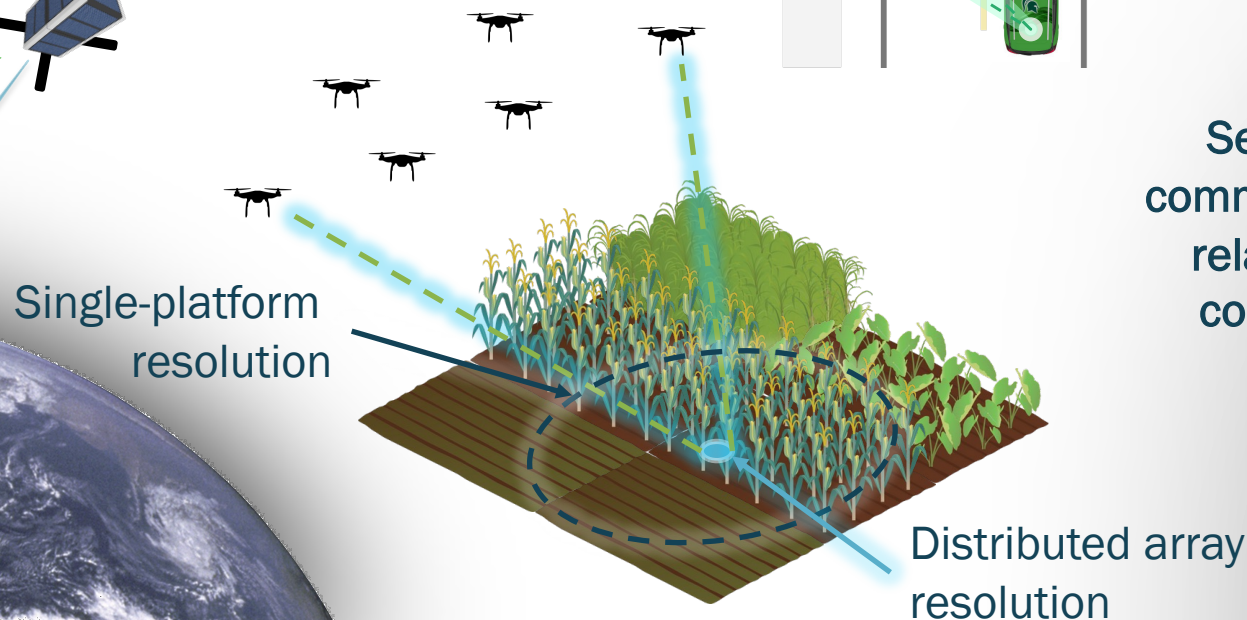
## Next Generation Satellite Cellular Networks



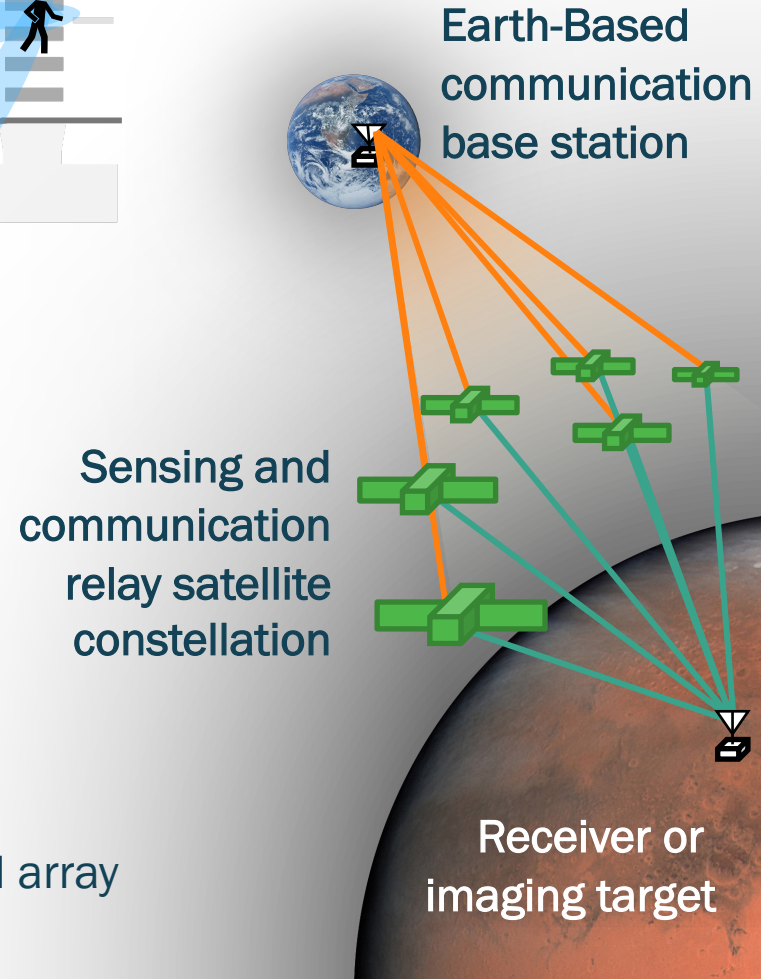
## Distributed V2X Sensing

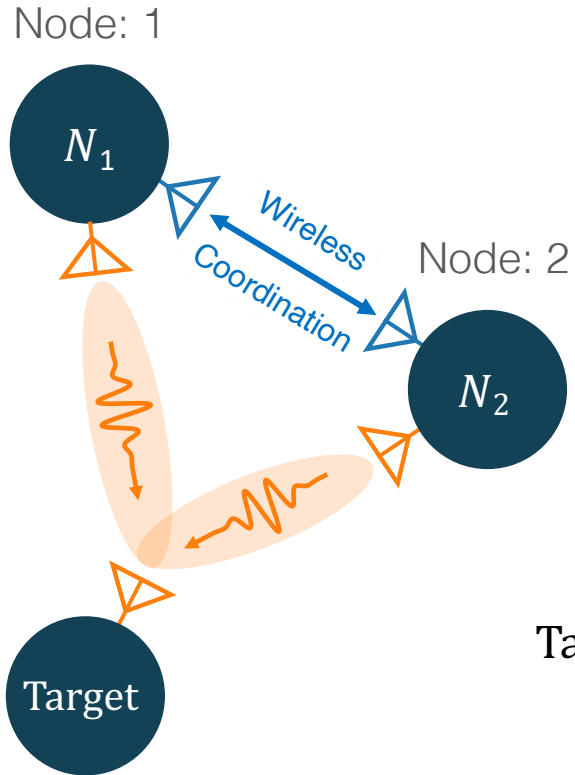


## Precision Agricultural Sensing

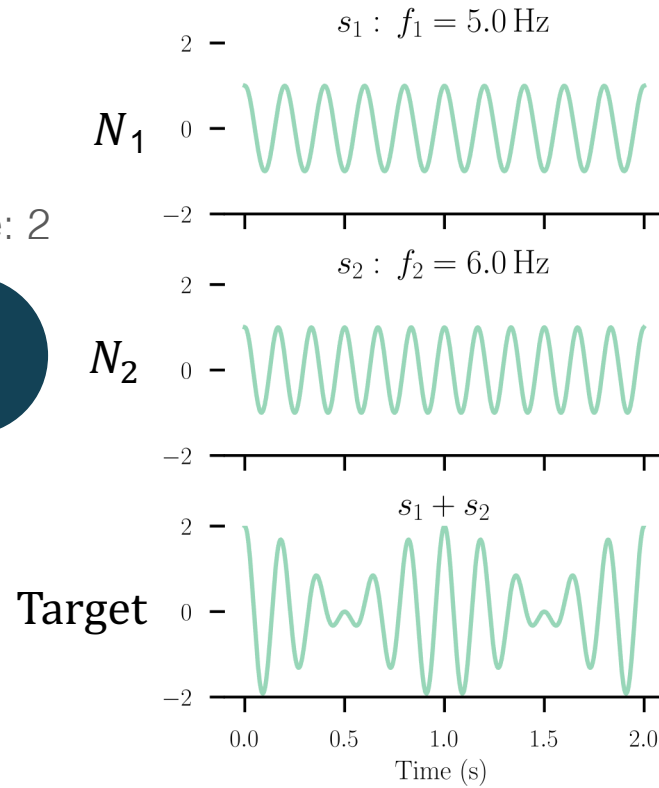


## Space Communication and Remote Sensing

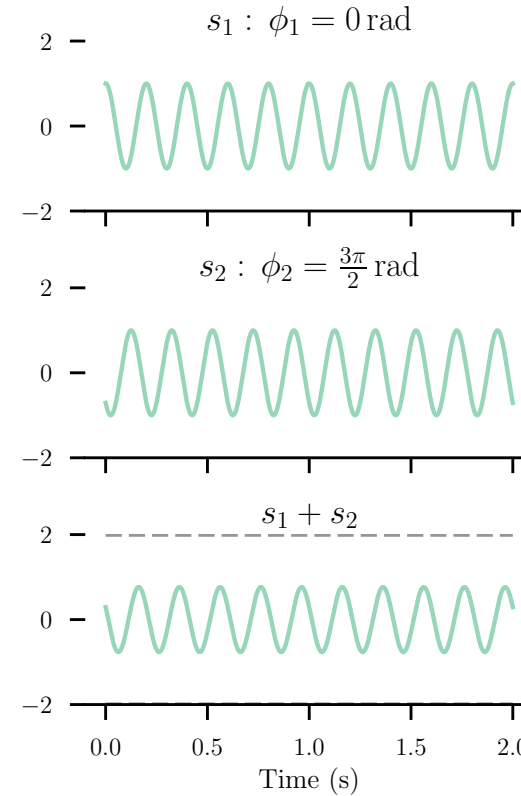




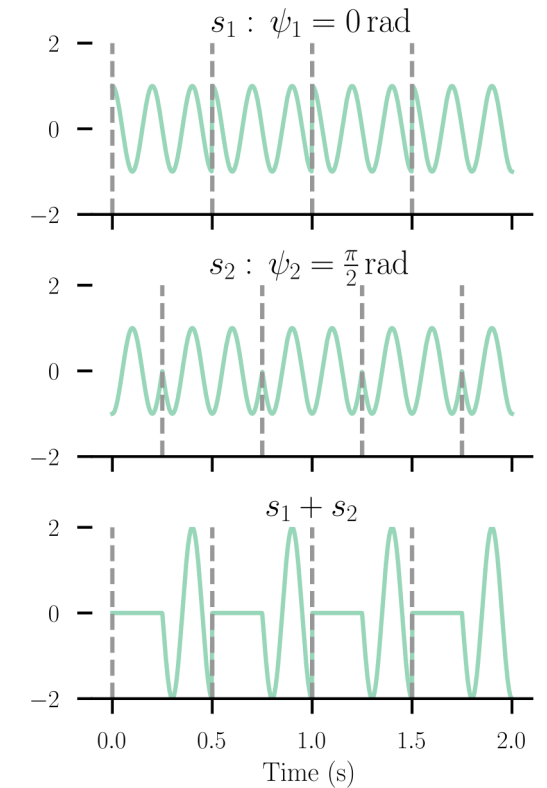
## Frequency Synchronization



## Phase Alignment



## Time Synchronization



$$s_1 + s_2 = \sum_{n=1}^2 \alpha_n(t - \delta t_n) \exp\{j[2\pi(f + \delta f_n) + \phi_n]\}$$

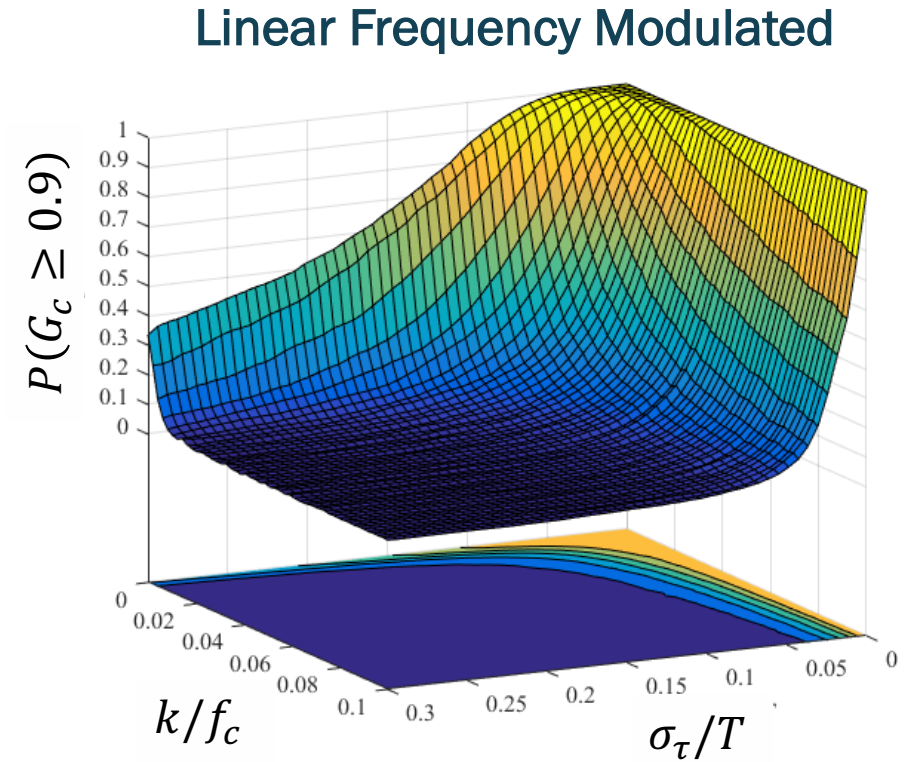
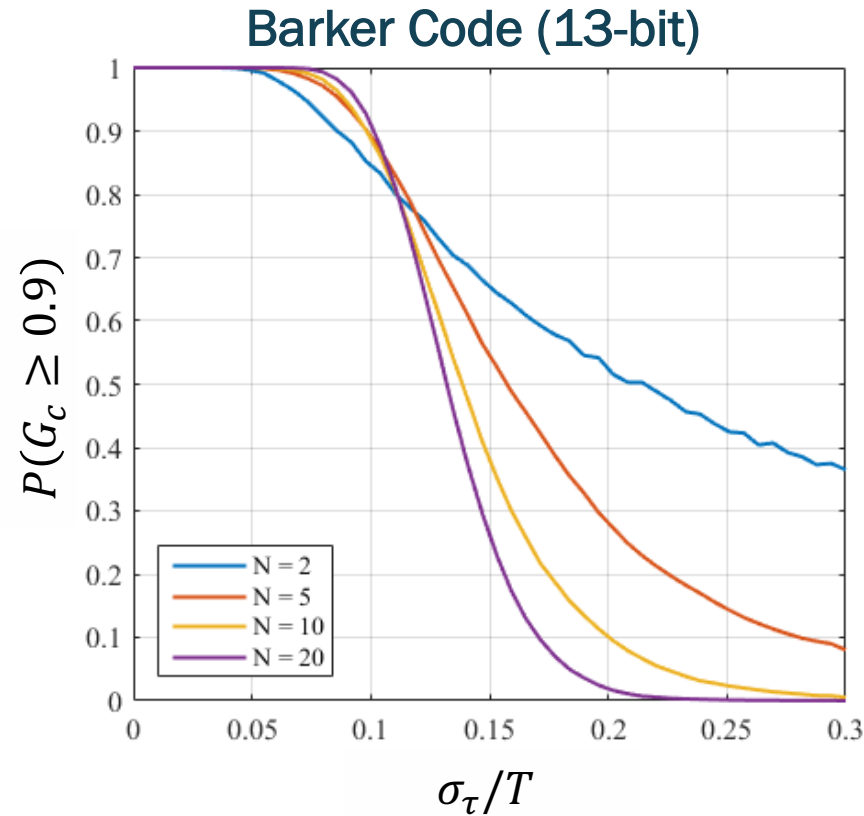
Probability of coherent gain:

$$P(G_c \geq X)$$

where

$$G_c = \frac{|s_r s_r^*|}{|s_i s_i^*|}$$

- $s_r$ : received signal
- $s_i$ : ideal signal



- [1] J. A. Nanzer, R. L. Schmid, T. M. Comberiate and J. E. Hodkin, "Open-Loop Coherent Distributed Arrays," in IEEE Transactions on Microwave Theory and Techniques, vol. 65, no. 5, pp. 1662-1672, May 2017, doi: 10.1109/TMTT.2016.2637899.
- [2] P. Chatterjee and J. A. Nanzer, "Effects of time alignment errors in coherent distributed radar," in Proc. IEEE Radar Conf. (RadarConf), Apr. 2018, pp. 0727-0731.

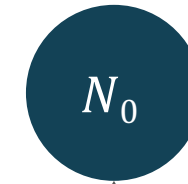
- Local time at node  $n$ :

$$T_n(t) = t + \delta_n(t) + v_n(t)$$

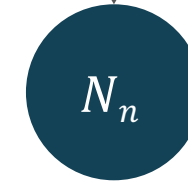
- $t$  : true time
  - $\delta_n(t)$ : time-varying offset from global true time
  - $v_n(t)$ : other zero-mean noise sources
  - $\Delta_{0n}(t) = T_0(t) - T_n(t)$
- Goal: estimate and compensate for  $\Delta_{0n}$

Relative Clock Alignment

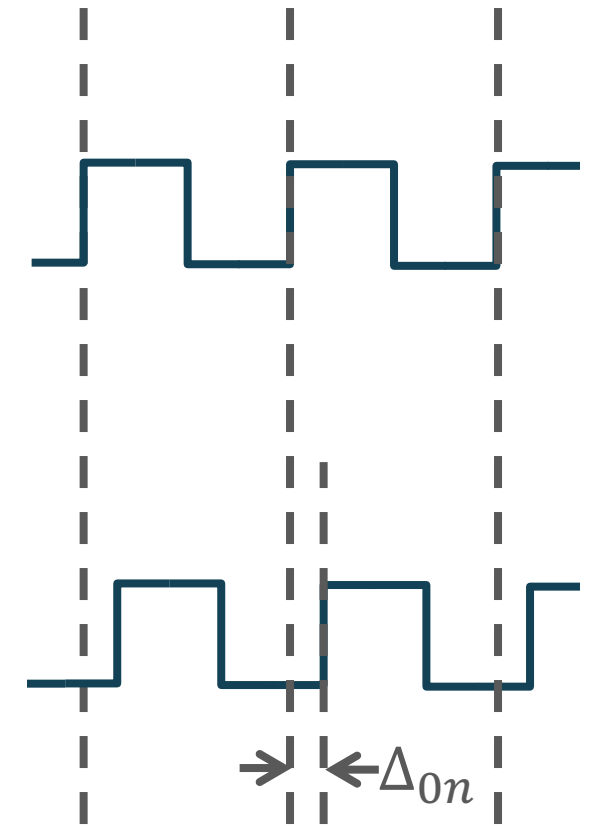
Node: 0



$R$



Node:  $n$

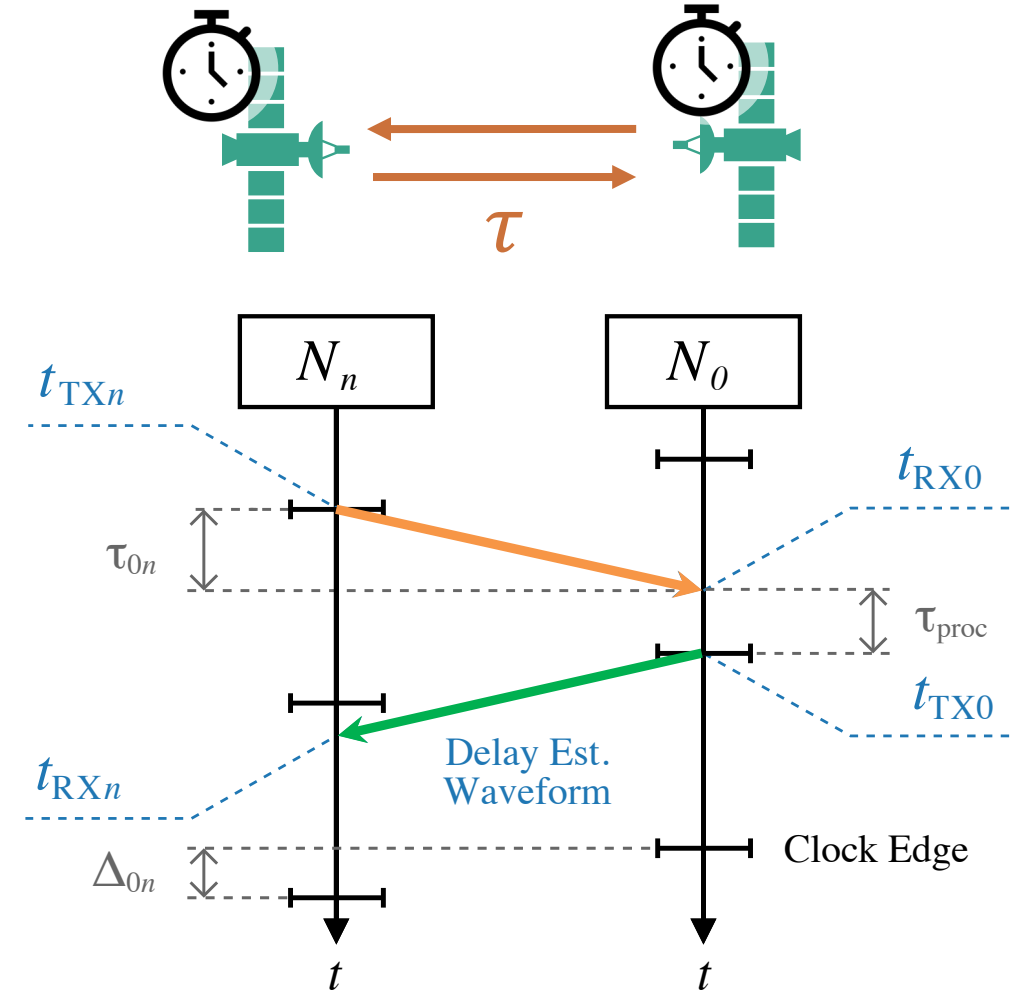


## Two-Way Time Synchronization

- Assumptions:
  - Link is quasi-static and reciprocal during the synchronization epoch
- Timing skew estimate:

$$\Delta_{0n} = \frac{(T_{RX0} - T_{TXn}) - (T_{RXn} - T_{TX0})}{2}$$

For compactness of notation:  $T_m(t_{TXn}) = T_{TXn}$



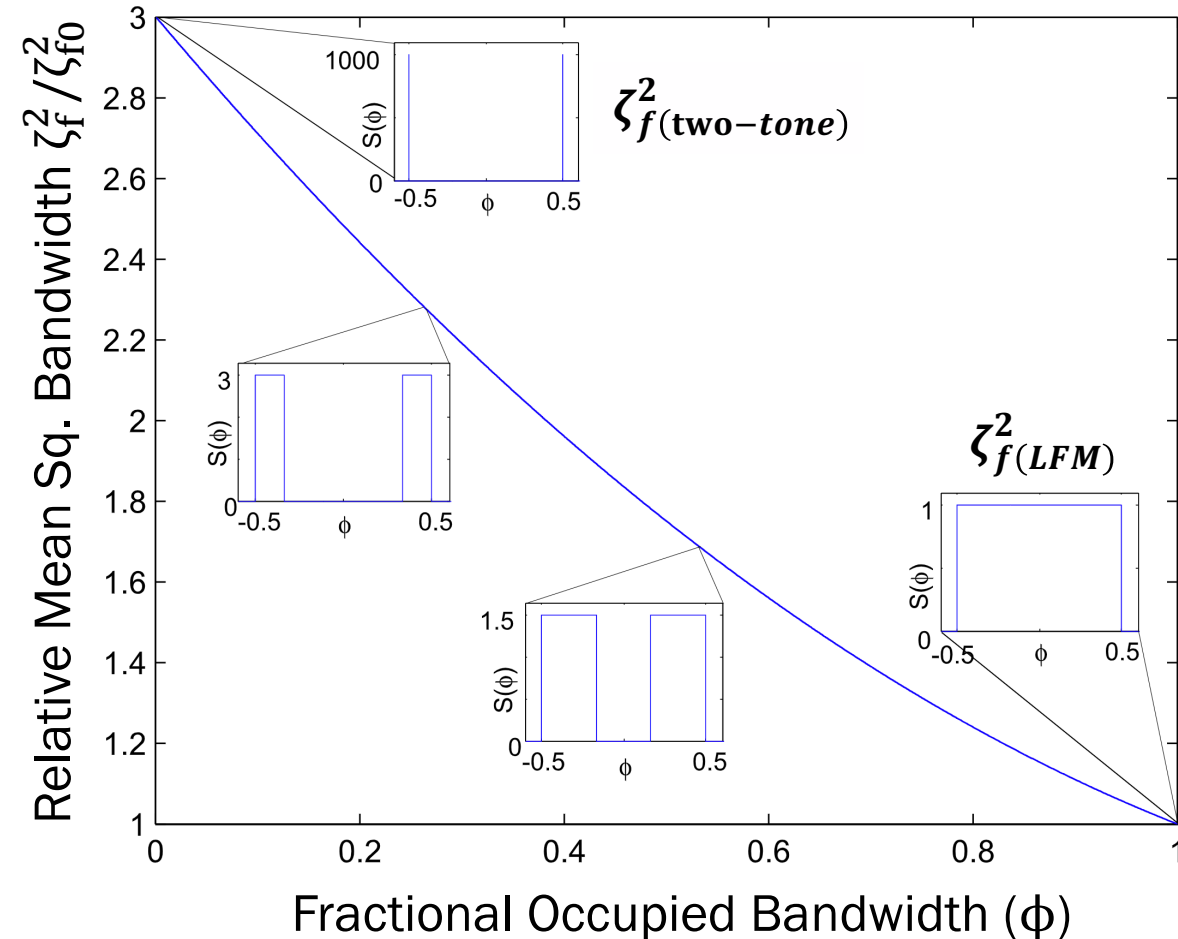
- The delay accuracy lower bound (CRLB) for time is given by

$$\text{var}(\hat{\tau} - \tau) \geq \frac{1}{2\zeta_f^2} \cdot \frac{N_0}{E_s}$$

- $\zeta_f^2$ : mean-squared bandwidth
- $N_0$ : noise power spectral density
- $E_s$ : signal energy

$$\frac{E_s}{N_0} = \tau_p \cdot \text{SNR} \cdot \text{NBW}$$

- $\tau_p$ : integration time
- SNR: signal-to-noise ratio
- NBW: noise bandwidth



[3] J. A. Nanzer and M. D. Sharp, "On the Estimation of Angle Rate in Radar," *IEEE T Antenn Propag*, vol. 65, no. 3, pp. 1339–1348, 2017, doi: 10.1109/tap.2016.2645785.

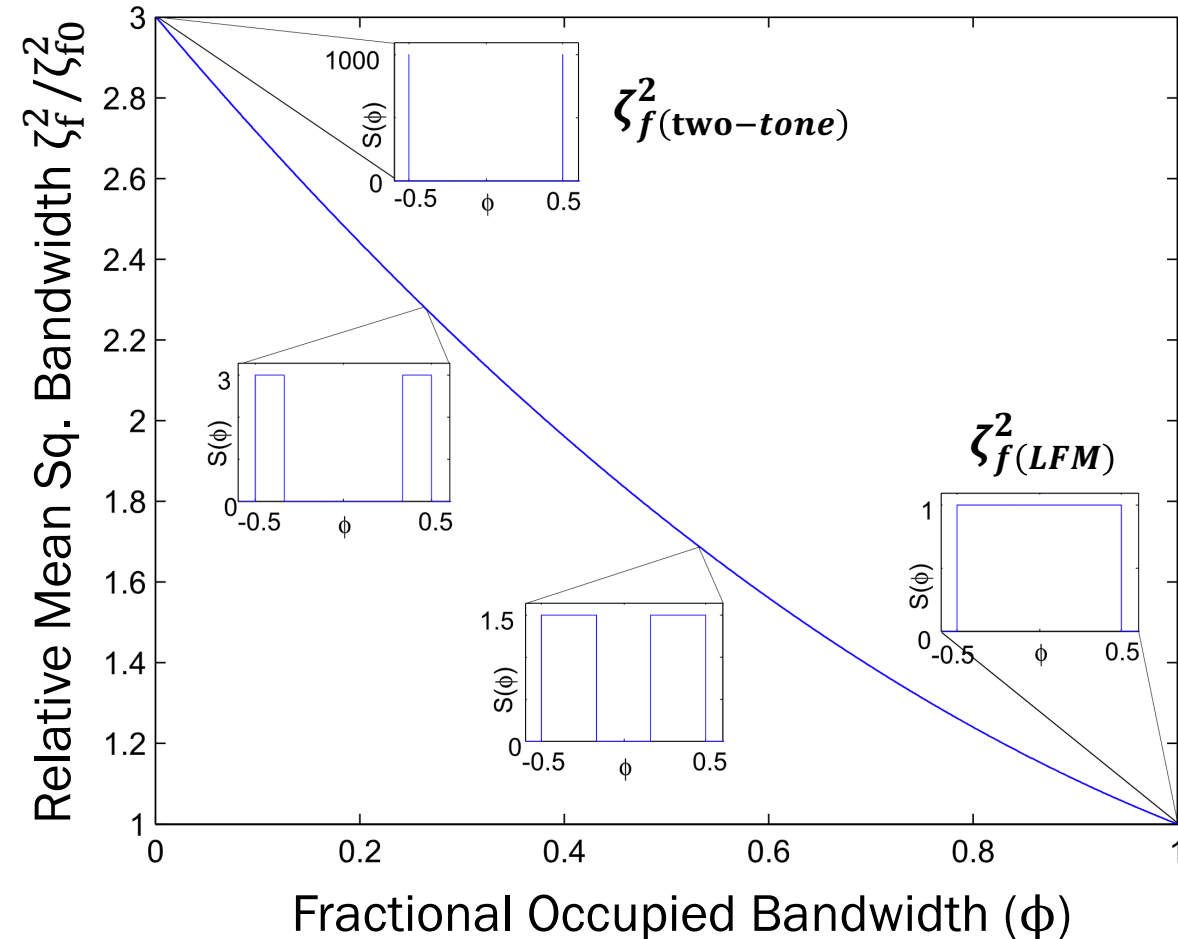
$$\text{var}(\hat{\tau} - \tau) \geq \frac{1}{2\zeta_f^2} \cdot \frac{N_0}{E_s}$$

- For constant-SNR, maximizing  $\zeta_f^2$  will yield improved delay estimation

$$\zeta_f^2 = \int_{-\infty}^{\infty} (2\pi f)^2 |G(f)|^2 df$$

- $\zeta_{f(LFM)}^2 = (\pi \cdot \text{BW})^2 / 3$

- $\zeta_{f(\text{two-tone})}^2 = (\pi \cdot \text{BW})^2$



[3] J. A. Nanzer and M. D. Sharp, "On the Estimation of Angle Rate in Radar," *IEEE T Antenn Propag*, vol. 65, no. 3, pp. 1339–1348, 2017, doi: 10.1109/tap.2016.2645785.

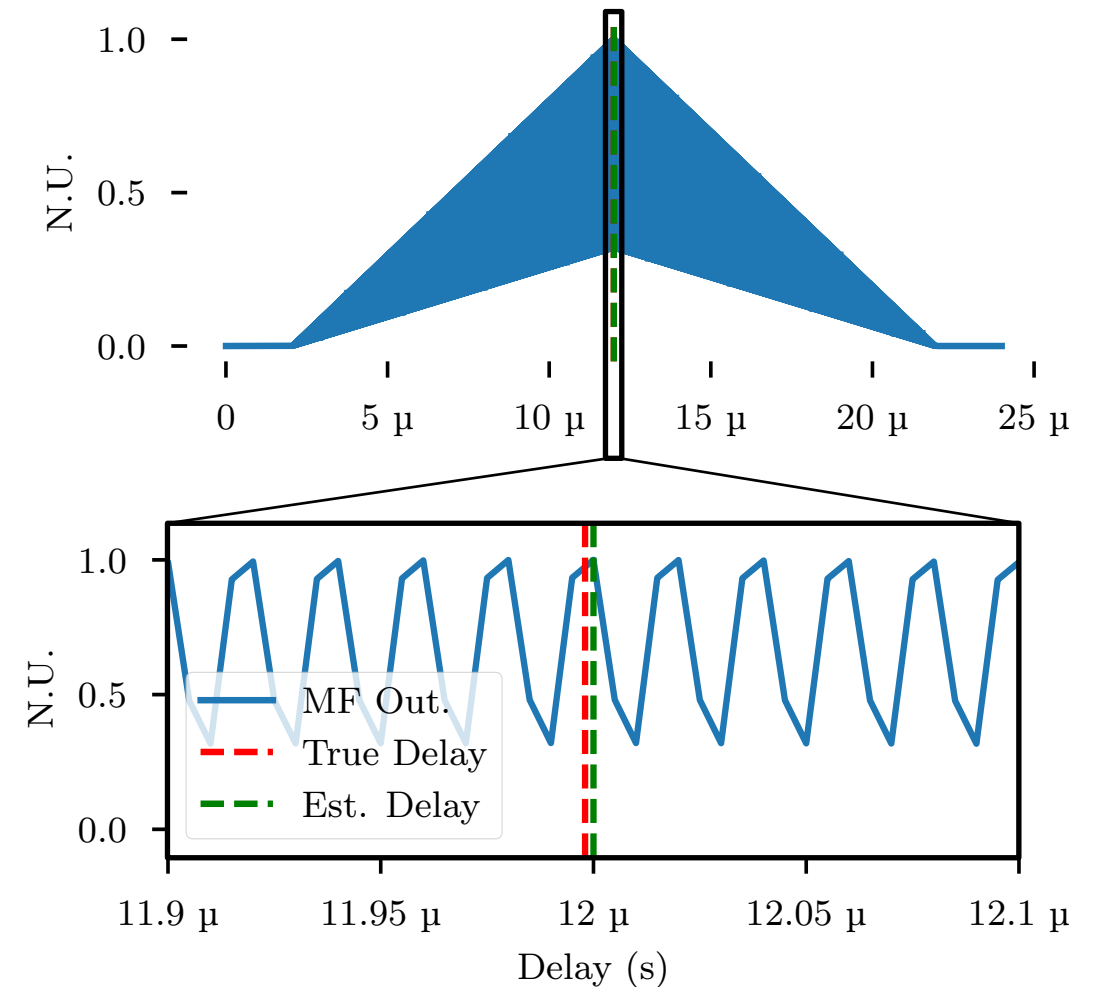


- Discrete matched filter (MF) used in initial time delay estimate

$$s_{MF}[n] = s_{RX}[n] \odot s_{TX}^*[-n]$$

$$= \mathcal{F}^{-1}\{S_{RX}S_{TX}^*\}$$

- Two-tone matched filter waveform is highly ambiguous
- High SNR or narrow-band pulse required to disambiguate peaks

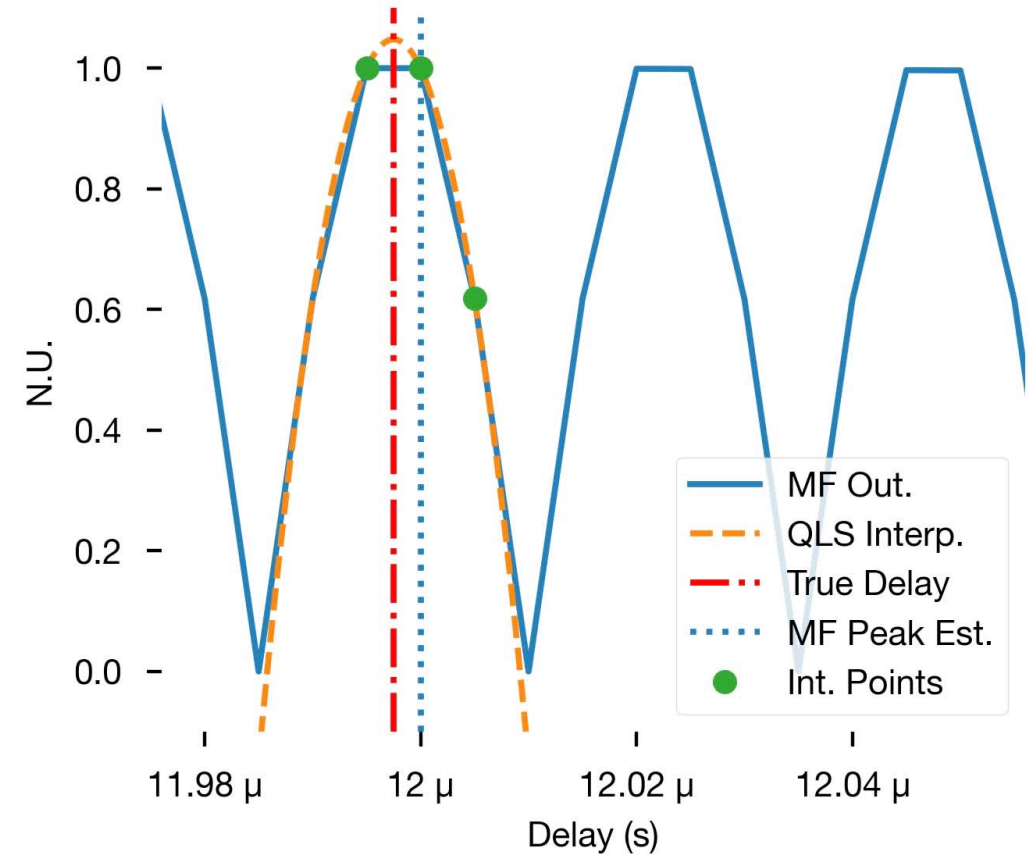


- MF causes estimator bias due to time discretization
- Refinement of MF obtained using Quadratic Least Squares (QLS) fitting to find true delay based on three sample points

$$\hat{\tau} = \frac{T_s}{2} \frac{s_{MF}[n_{\max} - 1] - s_{MF}[n_{\max} + 1]}{s_{MF}[n_{\max} - 1] - 2s_{MF}[n_{\max}] + s_{MF}[n_{\max} + 1]}$$

where

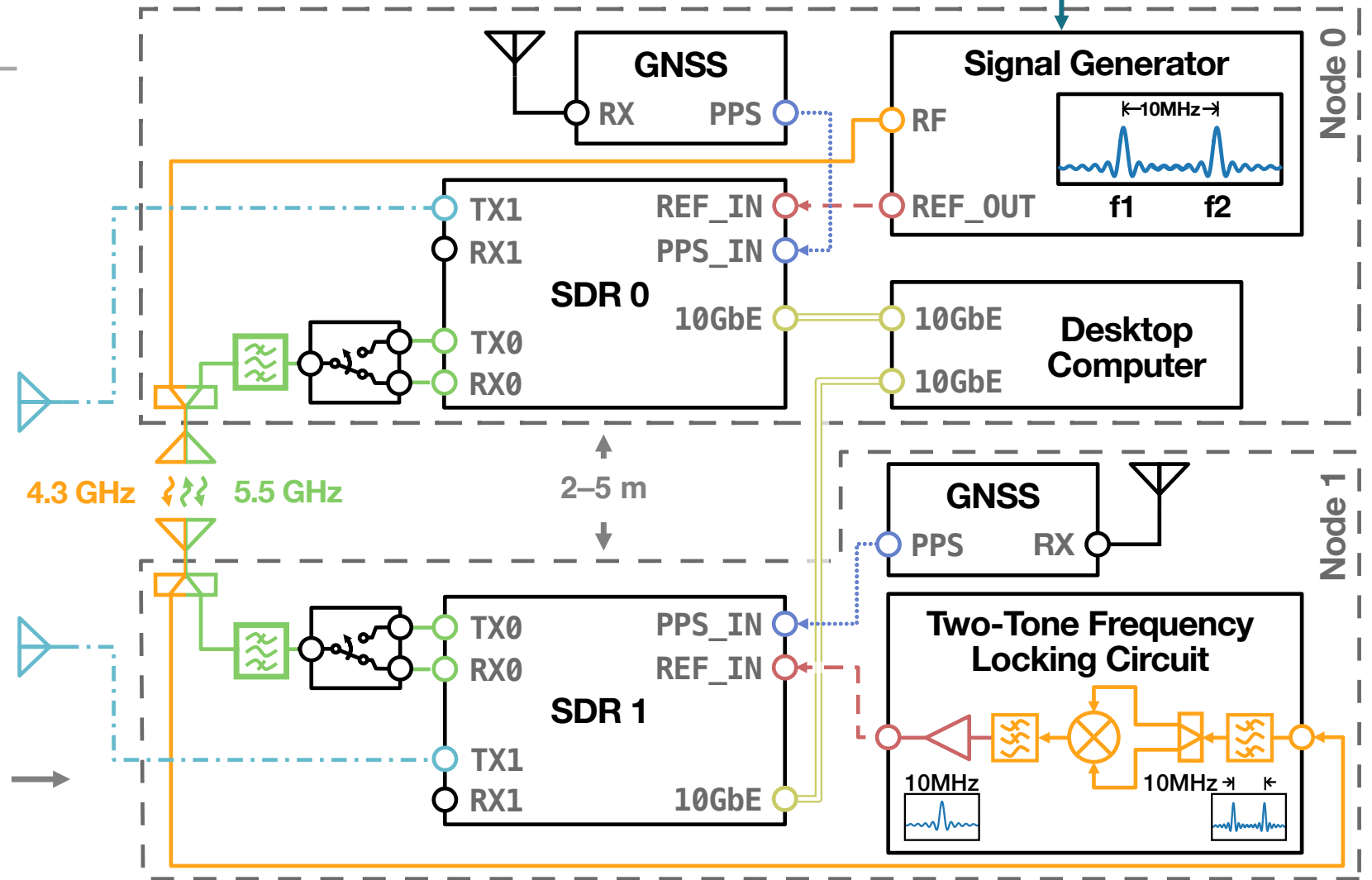
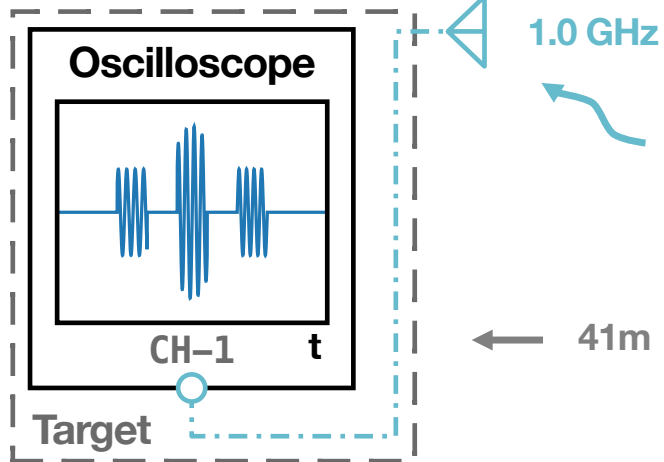
$$n_{\max} = \underset{n}{\operatorname{argmax}}\{s_{MF}[n]\}$$



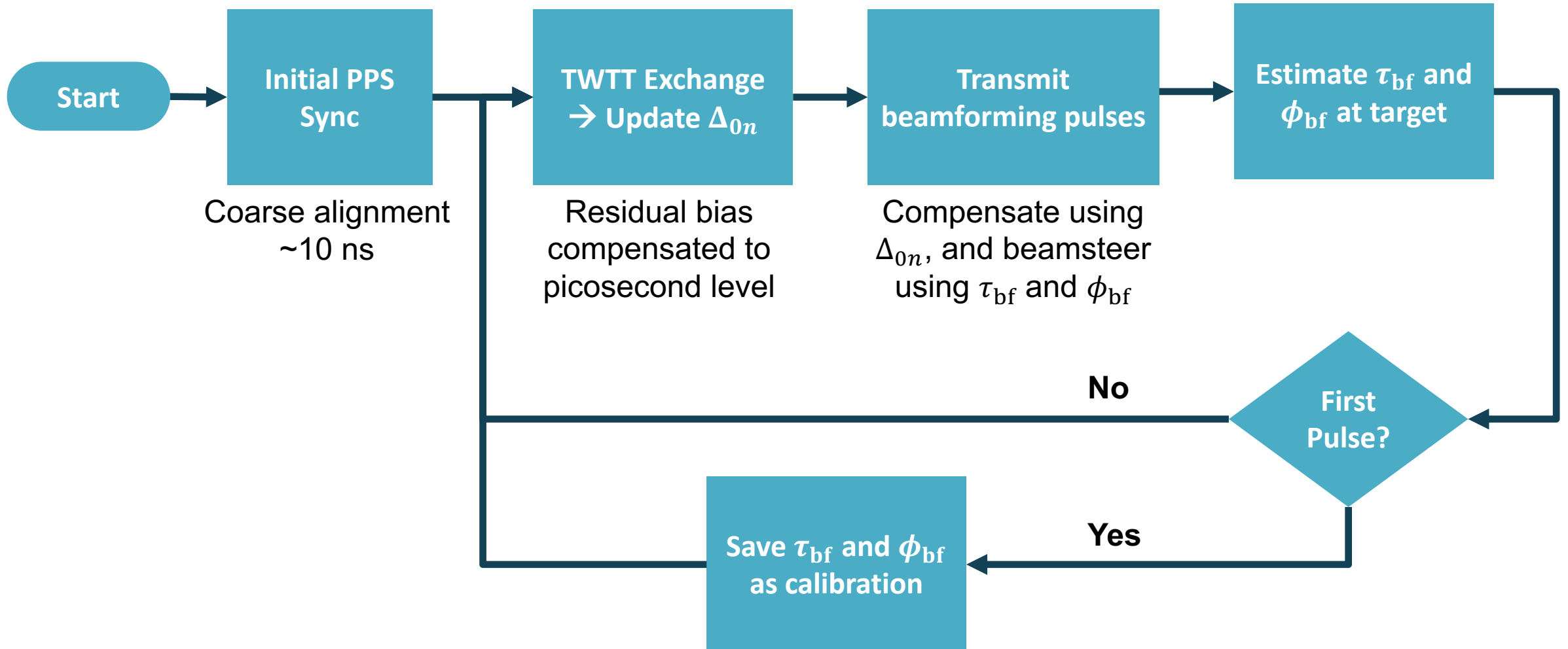
# System Configuration

## Legend

- Time Transfer Waveform
- Frequency Transfer Waveform
- - - 10 MHz Frequency Reference
- ⋯ PPS (coarse time sync)
- 10 GbE (data)
- - - Beamforming

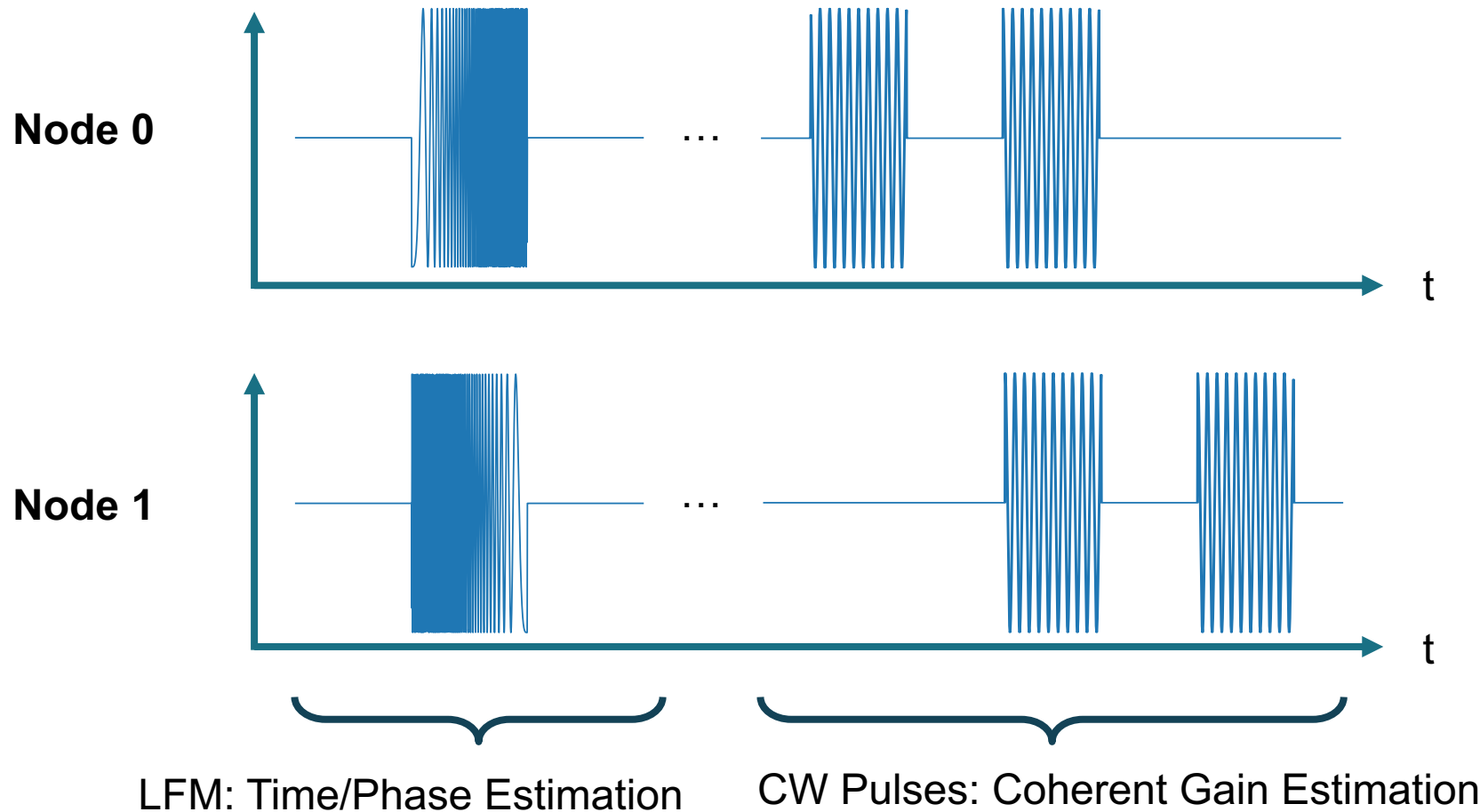


# System State Flow

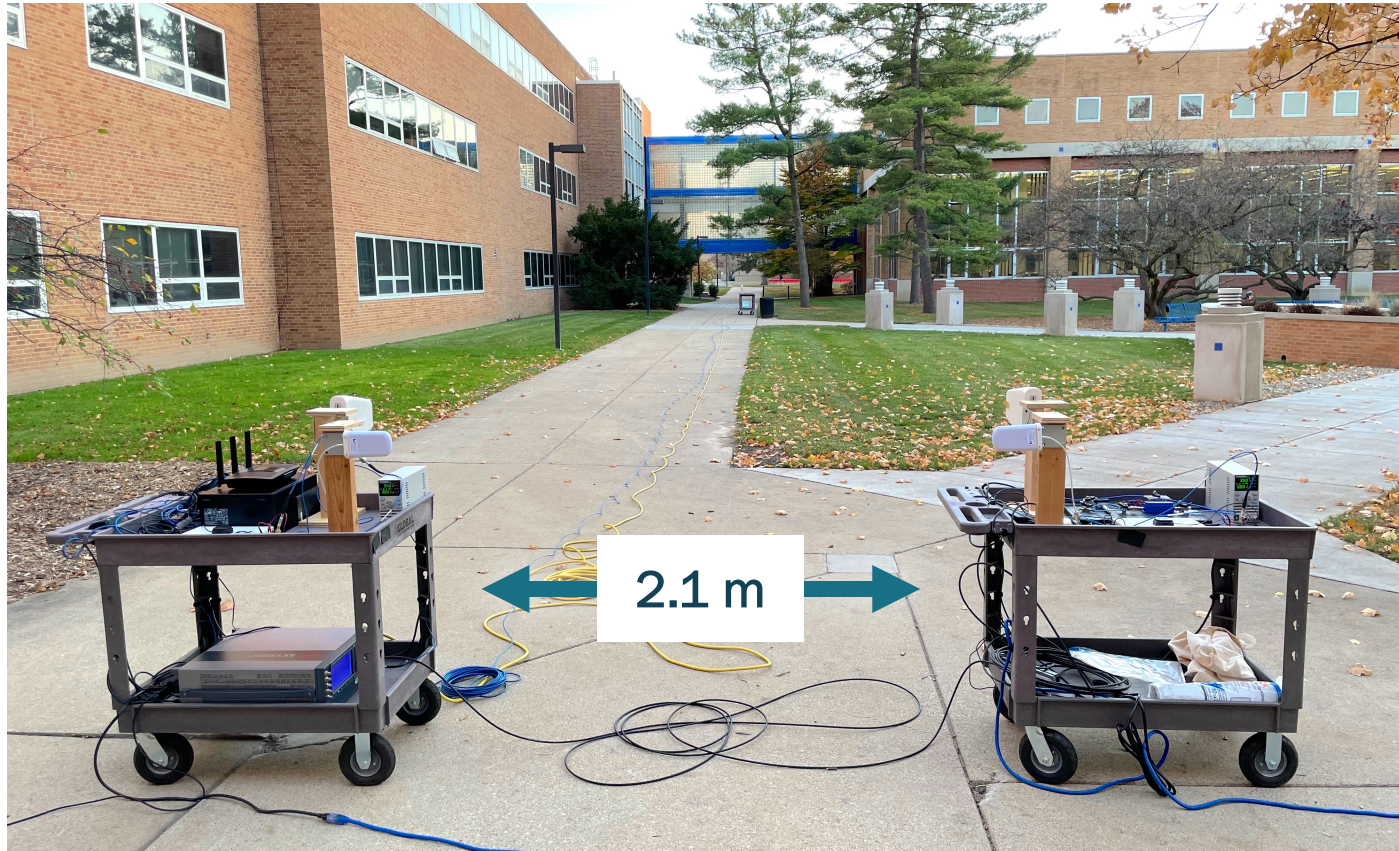


# Beamforming Waveforms

- Each node transmitted orthogonal LFMs followed by two CW pulses



# Beamforming Experiment



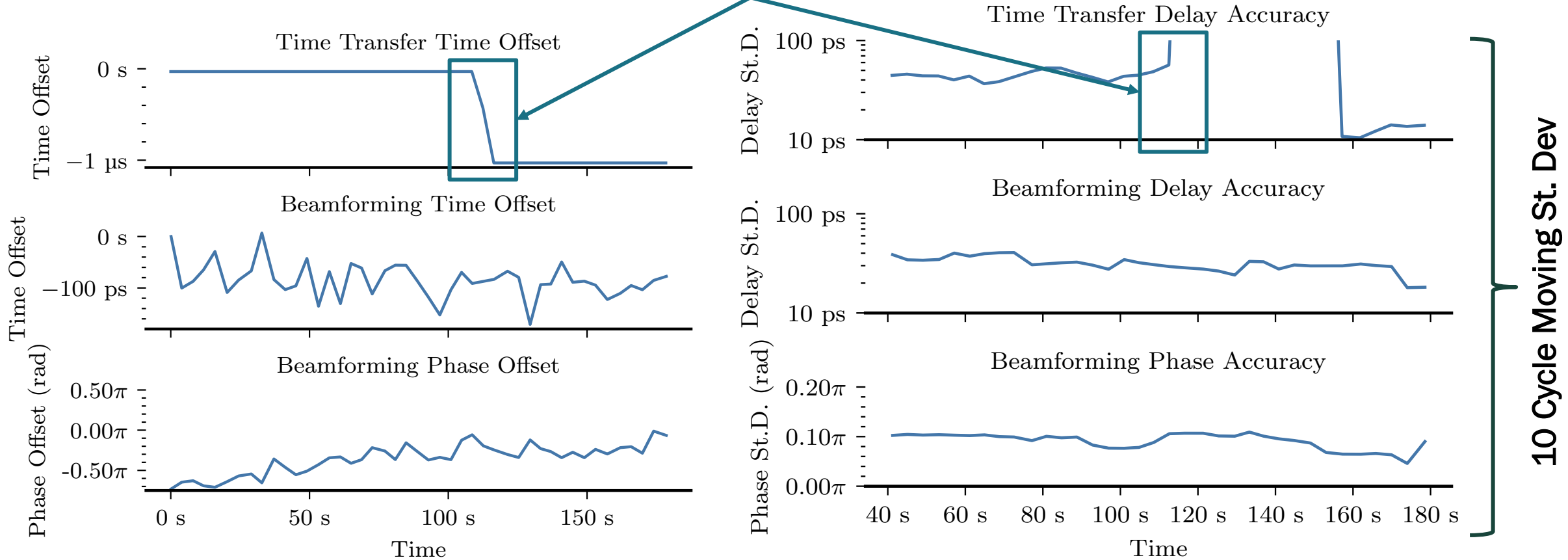
Transmit Nodes Setup



Target Node Setup (41 m downrange)

# Beamforming Experiment

Tested Frequency Transfer Failure



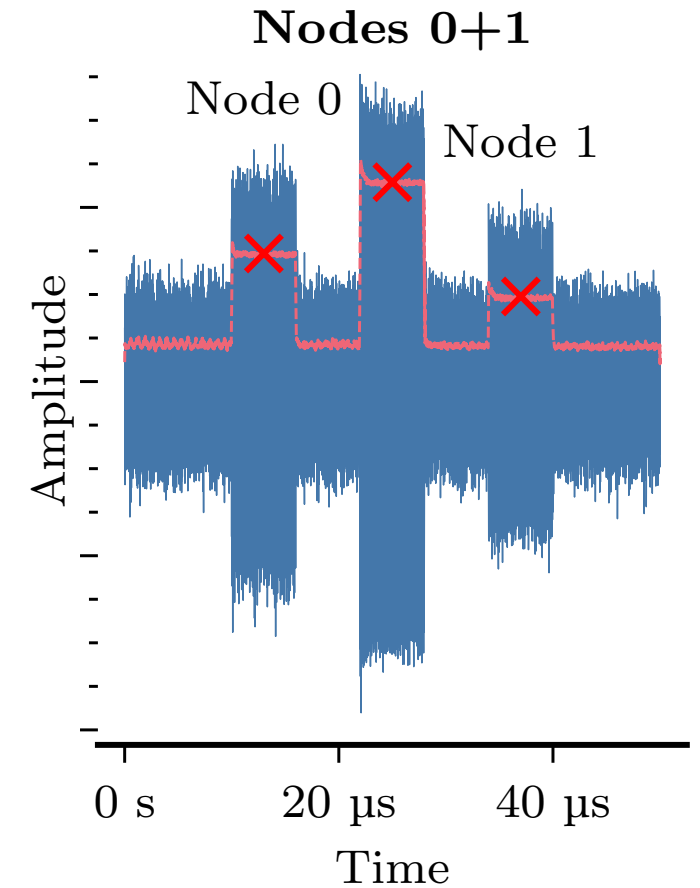
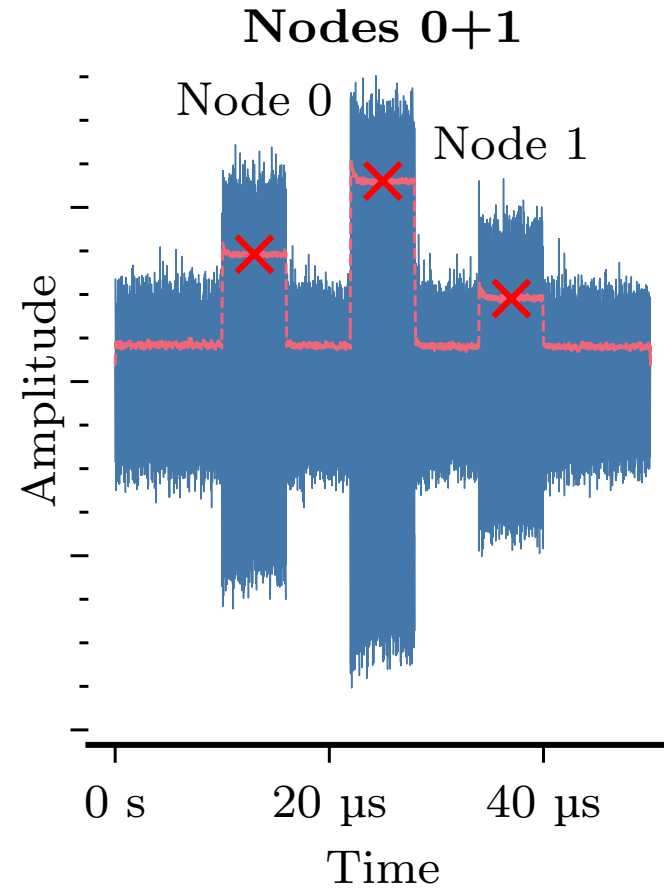
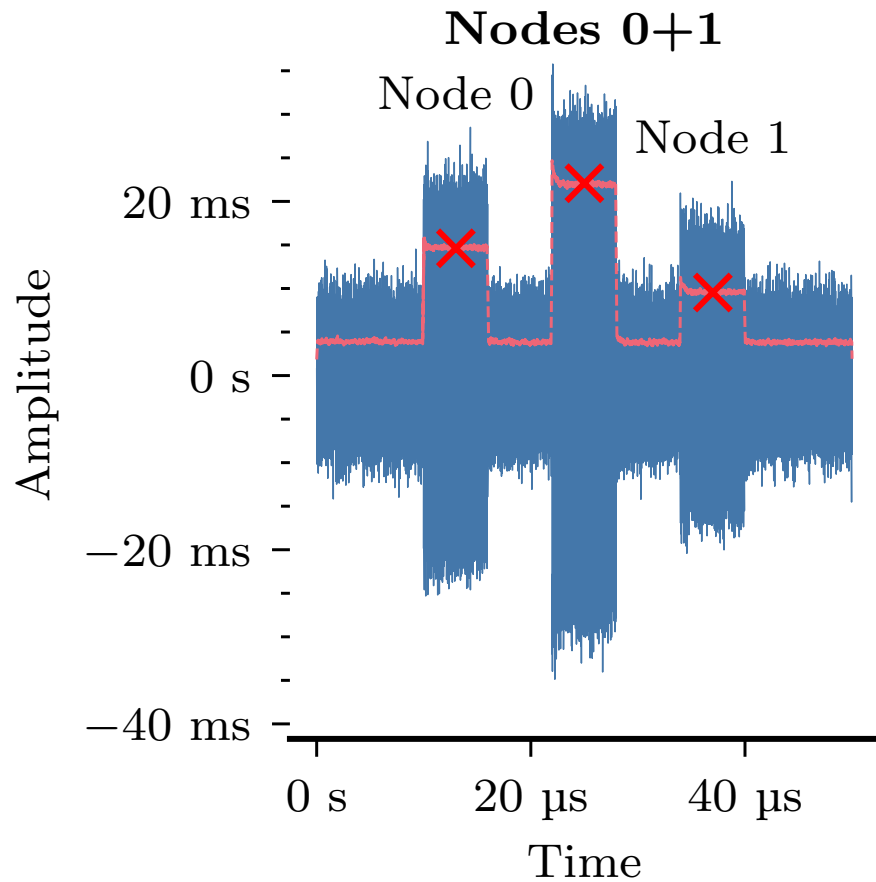
- Time Transfer SNR:  $\sim 23\text{dB}$
- Beamforming Std.:  $18 < \sigma_{bf} < 40 \text{ ps}$
- Throughput (BPSK):  $2.5 < b_{\text{max}} < 5.5 \text{ Gbps}$
- Cycle Time:  $\sim 4 \text{ s}$
- Phase Std.:  $0.04\pi < \sigma_{\phi} < 0.10\pi$
- Max Carrier Freq.:  $1.0 < f_{\text{max}} < 2.78 \text{ GHz}$

# Beamforming Experiment

Coherent Gain: 0.91

Coherent Gain: 0.95

Coherent Gain: 0.94





- **Discussed:**
  - High-accuracy time transfer technique using spectrally sparse two-tone waveforms
  - Two-step refinement and QLS bias compensation process
- **Demonstrated:**
  - fully wireless outdoor time-frequency synchronization and beamforming with  $G_c > 0.9$  over a 41 m

Internode Distance	Min. Time Transfer Std.	Min. Beamforming Std.	Max. Throughput (BPSK; $G_c \geq 0.9$ )	Max. Carrier Frequency $P(G_c \geq 0.9) \geq 0.9$
2.1 m	10.47 ps	18.00 ps	5.56 Gbps	2.78 GHz
5.0 m	14.79 ps	24.02 ps	4.16 Gbps	2.08 GHz

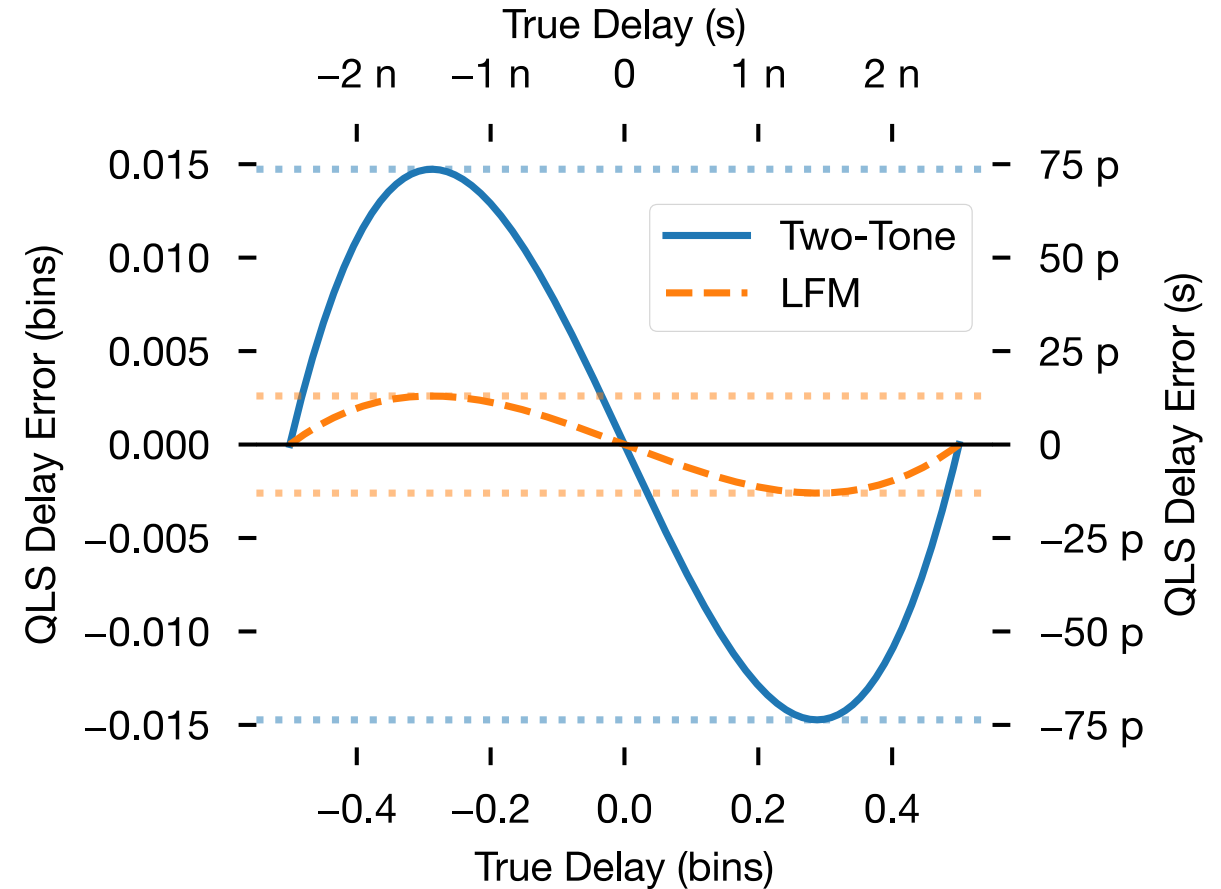
# Questions

Thank you to our project sponsors and collaborators:

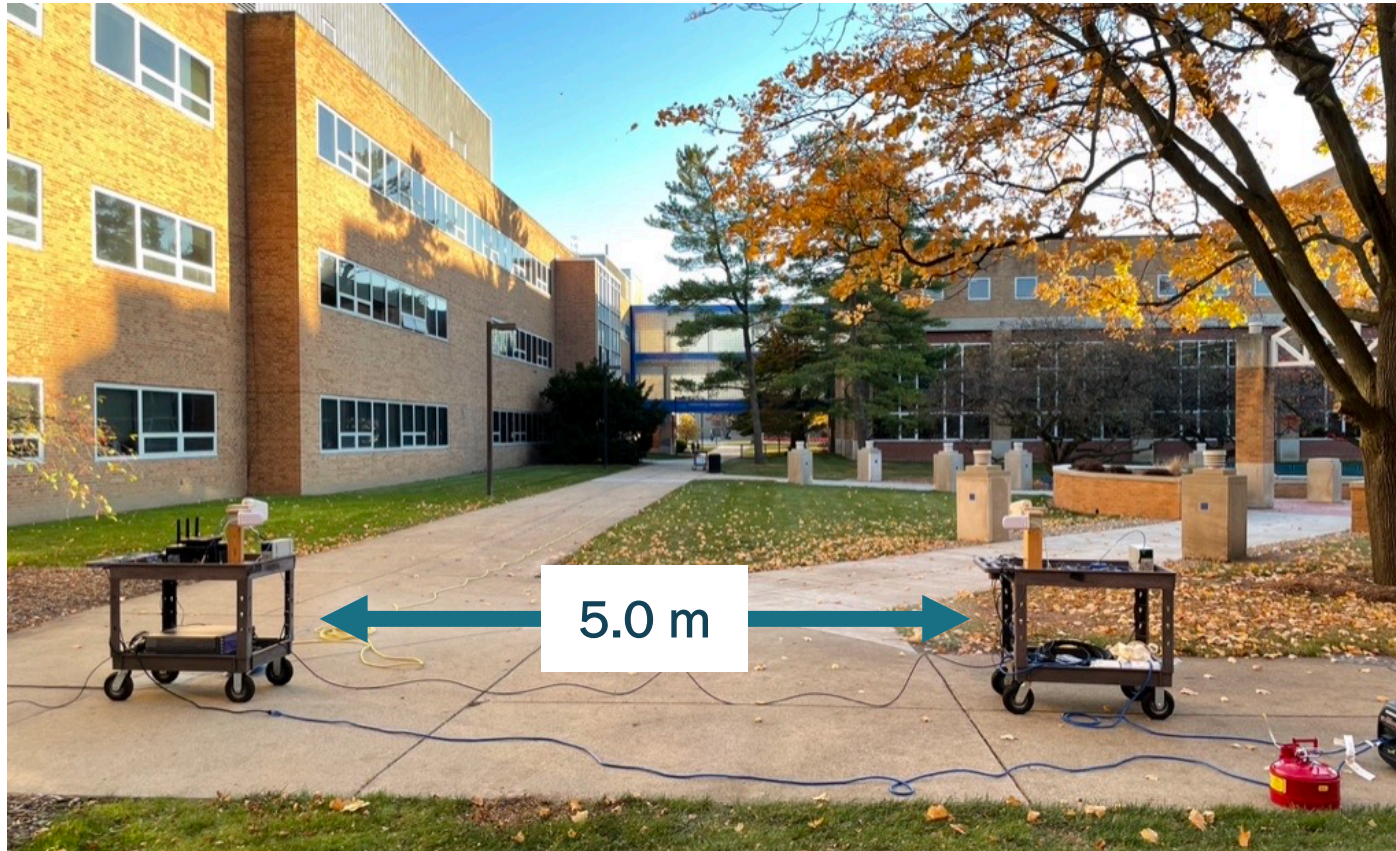


# Backup Slides

- QLS results in small residual bias due to an imperfect representation of the underlying MF output
- Residual bias is a function of waveform and sample rate
- Can be easily corrected via lookup table



# Baseline 5.0 m



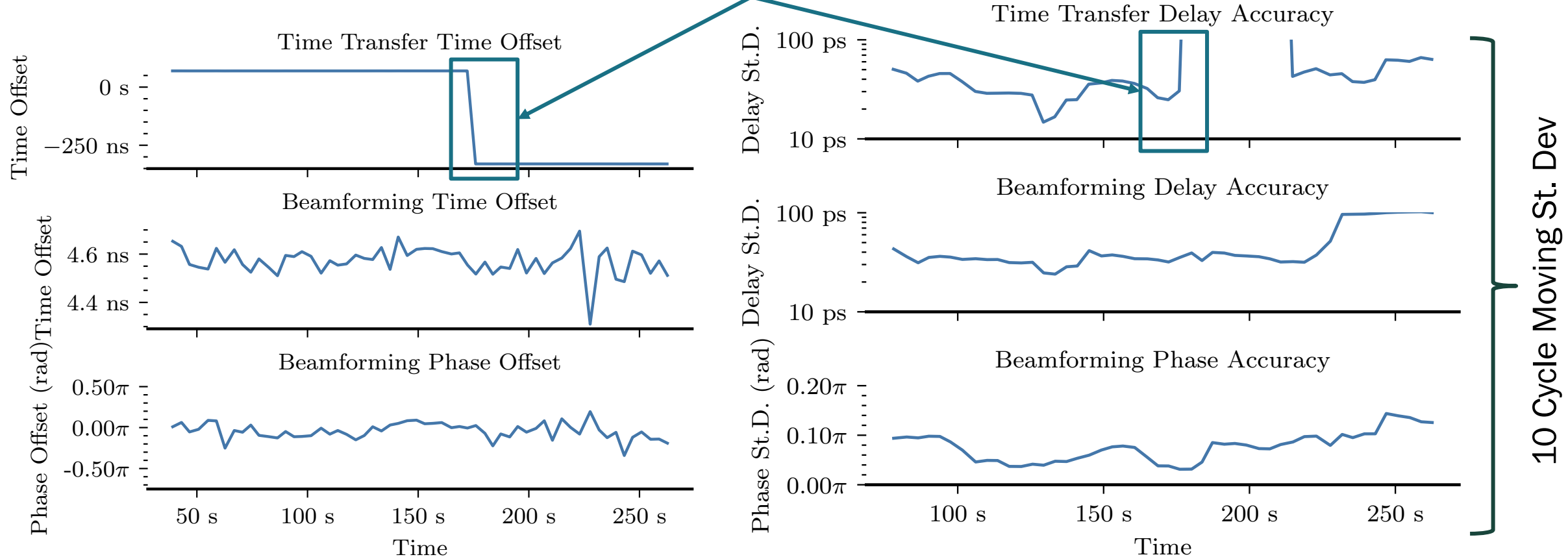
Transmit Nodes Setup



Target Node Setup (41 m downrange)

# Baseline 5.0 m

Tested Frequency Transfer Failure



- Time Transfer SNR:  $\sim 23\text{dB}$
- Beamforming Std.:  $24 < \sigma_{bf} < 100 \text{ ps}$
- Throughput (BPSK):  $1.0 < b_{\text{max}} < 4.16 \text{ Gbps}$
- Cycle Time:  $\sim 4 \text{ s}$
- Phase Std.:  $0.05\pi < \sigma_{\phi} < 0.10\pi$
- Max Carrier Freq.:  $0.67 < f_{\text{max}} < 2.08 \text{ GHz}$

# Baseline 5.0 m

Coherent Gain: 0.90

Coherent Gain: 0.92

Coherent Gain: 0.94

